

**LECTURE NOTES**  
**ON**  
**ELECTRICAL CIRCUITS**

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**B. Tech II Semester (IARE-R16)**

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# UNIT – I

## INTRODUCTION TO ELECTRICAL CIRCUITS

### 1.1 INTRODUCTION:

With increase in population the need for electricity also increases therefore it is necessary to rise number of electrical engineers. The electrical engineering mainly deals with generation , transmission and distribution of electricity.

Electrical circuits is the basic and fundamental subject which lays path to understand subjects related to generation , transmission and distribution of electricity.

In the first unit we shall deal with what is electrical circuit and formation of electrical circuit. Knowing or unknowing we come across electron in our life daily, studying the properties of these electrons leads to the terms voltage, current and power. Hence the basic definitions of voltage , current , power and energy are studied here.

### 1.2 CIRCUIT:

The electrical circuit consists of mainly three parts , they are -- source, connecting wire and load or sink.

Source : An source may be battery which forces electrons into the circuit.

Connecting wire : This is part which provides path for electrons to flow.

Load : The load may be bulb etc. when electrons flow through it an reaches the Source it glows .

If the electrons are provided closed path to flow, leads to current is called as **electrical circuit**.

### 1.3 BASIC DEFINITIONS:

**Voltage(V)** : The potential difference between force applied to two oppositely charged particles to bring them as near as possible is called as potential difference .( in electrical terminology it s voltage).

$$V = W / Q \text{ (v)}$$

$$v = dw / dq \text{ (v)}$$

v- volts , units of voltage.

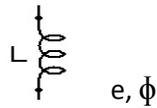
- Unit volt is defined as 1C of charge developed when 1 J of energy is applied.

**Current(I)** : The flow of electrons develops the current.

$$I = Q/t \text{ (A)}$$



Alternating current is allowed through such an element it induces Voltage in it.



Where,  $e = \text{emf induced}$

$\phi = \text{flux developed in it for current } i.$

Hence,  $e = L \, di/dt \text{ (v)}$ .

$L = \text{is the inductance of the coil (H)}$

H = henry units of inductance.

Unit H is the 1v of voltage induced in coil when current changing at rate of 1A/S .

by solving above equation , current flowing through coil is given as,

$$i = (1/L) \int v \, dt + i(0+).$$

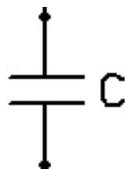
Energy stored in inductor,

$$W = \int e \cdot i \, dt = \int L \, di/dt \cdot i \, dt = (1/2) L i^2$$

### Properties:

- Inductor doesn't allow sudden changes in current.
- If DC supply is provided to inductor it acts as short circuit.
- Pure inductor is non-dissipative element i.e its internal resistance is zero.
- stores energy in the form of magnetic field.

**1.3.3 Capacitor :** two parallel plates oppositely charged separated by an dielectric medium constitutes an capacitor.



current flowing through capacitor, given as

$$i = c \, dv/dt$$

when some voltage  $v$  is applied ,  $i$  is the

$c =$  capacitance of the capacitor.(F)

Farad is the unit of capacitance, 1F is the when 1A

Flow if 1v applied for 1S.

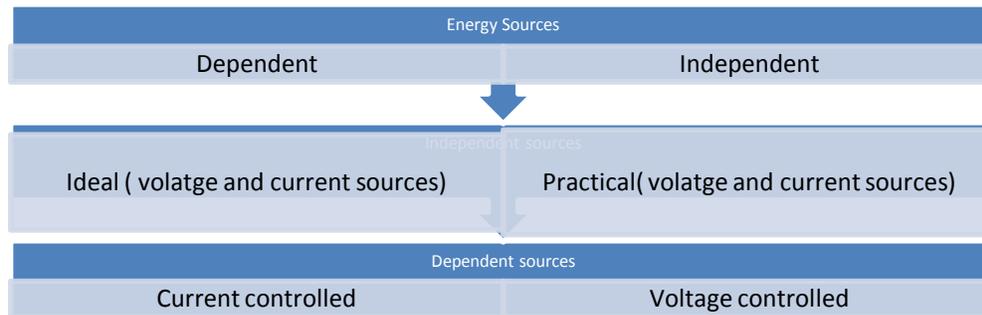
Volatge across capacitor is given as,  $v = (1/c) \int i dt + v(0+)$ .

Energy stored in capacitor is ,  $w = \int v.i dt = \int c dv/dt. i dt. = (1/2) cv^2$

### Properties:

- capacitor doesn't allow sudden changes in voltage.
- If DC supply is provided to capacitor it acts as open circuit.
- Pure capacitor is non-dissipative element i.e its internal resistance is zero.
- stores energy in the form of electric field.

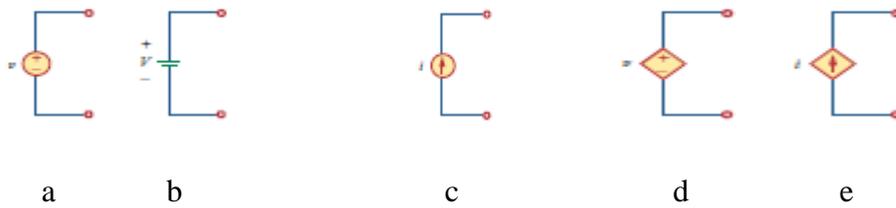
### 1.4 ENERGY SOURCES:



**Ideal sources:** These are one zero internal resistance their same will appear at terminals .

**Practical sources:** These are one with internal resistance and there is a drop at Terminal value than actual value applied.

<b>Ideal sources</b>	<b>Practical sources</b>
Current source : its parallel internal resistance is zero.  $I_t = I_s$ $I_t$ - terminal current $I_s$ - applied current	Current source : its parallel internal resistance is finite.  $I_t = I_s - (V_s / R_i)$ $I_t$ - terminal current $I_s$ - applied current $R_i$ -internal resistance
Voltage source : its series internal resistance is zero.  $V_t = V_s$ $V_t$ - terminal voltage $V_s$ - applied voltage	Voltage source : its series internal resistance is zero.  $V_t = V_s - I_s.R_v$ $V_t$ - terminal voltage $V_s$ - applied voltage $R_v$ -internal resistance



a – voltage source    b – voltage source    c – current source  
 d – voltage controlled source    e – current controlled source.

### 1.5 TYPES OF ELEMENTS:

**Active and passive elements:** Elements which deliver power are active and which receive power are passive.

**Eg:** voltage and current source for active elements.  
 R, L, C are passive elements.

**Uni-lateral and bi-lateral elements:** If the V-I characteristics are different for different directions of current they are called as uni-lateral otherwise bi-lateral elements.

**Eg:** diode, transistor etc for uni-lateral elements.  
 R for bi-lateral elements.

**Linear and non-linear elements:** elements which obey Ohm's law are called as linear otherwise non-linear.

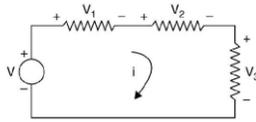
**Eg:** R for linear elements.  
 L, C are non-linear elements.

**Lumped and distributed:** Elements which are small in size are lumped and which are distributed throughout the line are distributed elements.

**Eg:** cable wire for distributed elements.  
 R, L, C in lab are lumped elements.

### 1.6 KIRCHOFF'S LAW:

**Kirchoff's voltage law (KVL):** States that algebraic sum of voltages in an loop is equal to zero.



$$\sum v = 0.$$

$$\begin{aligned} V &= V_1 + V_2 + V_3 \\ \text{Where, } V_1 &= i.R_1 \\ V_2 &= i.R_2 \\ V_3 &= i.R_3, \quad \text{from which} \end{aligned}$$

$$i = V / (R_1 + R_2 + R_3) = V_s / R_t$$

V = source voltage

i = source current

R<sub>t</sub> = equivalent or total resistance of circuit = R<sub>1</sub> + R<sub>2</sub> + R<sub>3</sub>

### Voltage division rule:

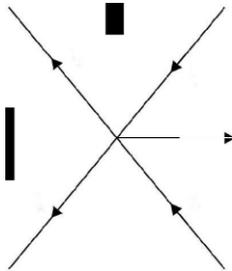
$$V_1 = i.R_1$$

We know that ,  $i = V / (R_1 + R_2 + R_3) = V_s / R_t$

Substituting i in V<sub>1</sub>,  $V_1 = V_s / R_t * R_1$ .

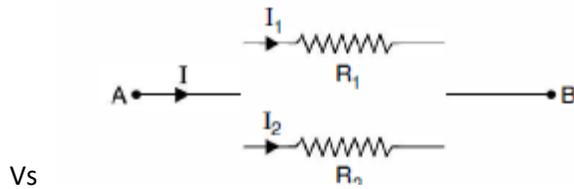
$$\begin{aligned} \text{Similarly, } V_2 &= V_s / R_t * R_2. \\ V_3 &= V_s / R_t * R_3. \end{aligned}$$

**Kirchoff's current law(KCL):** States that sum of the current entering junction is equal to sum of the leaving the junction.



Let  $i_1, i_2$  are entering currents and  $i_3, i_4$  are leaving currents, then

$$i_1 + i_2 = i_3 + i_4$$



### Current division rule:

Let  $V_s$  be the voltage at node A,  $I$  is the source current

$$I_1 = V_s / R_1$$

$$I_2 = V_s / R_2$$

Applying KCL at node A,  $I = I_1 + I_2 = V_s / R_1 + V_s / R_2$

$$V_s = I \cdot [ 1 / (1/R_1) + (1/R_2)] = I \cdot R_t$$

$$R_t = [ 1 / (1/R_1) + (1/R_2)] = R_1 \cdot R_2 / (R_1 + R_2)$$

$$I_1 = I \cdot R_2 / (R_1 + R_2).$$

$$I_2 = I \cdot R_1 / (R_1 + R_2).$$

## 1.7 NETWORK REDUCTION TECHNIQUES:

An circuit ia one with an loop , where as network is one more than one loop. An circuit is always closed one, where as network can be either closed or opened circuited. Now let us different techniques to solve networks.

### 1.7.1 Source Transformation:

To solve some of the network it may be necessary to convert voltage source to current source and vice-versa.

Let us consider  $V_s$  is source value and its internal resistance in series is  $R_v$  across a-b terminals,

If a-b are open circuited,  $V_{oc} = V_s$

If a-b are short circuited,  $I_{sc} = V_s / R_v$

Let us consider  $I_s$  is source value and its internal resistance in parallel is  $R_i$  across a-b terminals,

If a-b are open circuited,  $V_{oc} = I_s \cdot R_i$

If a-b are short circuited,  $I_{sc} = I_s$

Equating above two conditions.  $V_s = I_s \cdot R_i$

$$I_s = V_s / R_v$$

From above two conditions,  $I_s \cdot R_i = I_s \cdot R_v$

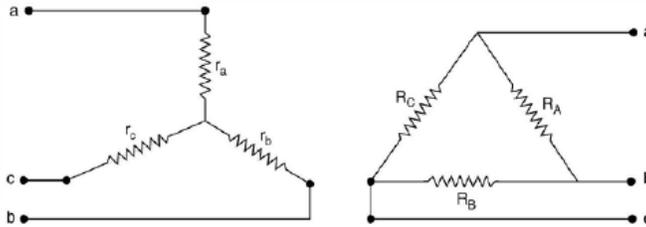
$$R_i = R_v$$

Means when source transformation is done their internal resistance will not change.

## **UNIT – II**

# **ELECTRICAL CIRCUITS ANALYSIS**

## 2.1 Star –Delta Transformations:



First figure shows elements connected in star and other elements connected in delta. Network involved such type of connections may be complex, hence we may require these transformations for easy solving of networks.

In star connection,

$$R_{ab} = (r_a + r_b)$$

$$R_{bc} = (r_c + r_b)$$

$$R_{ca} = (r_a + r_c)$$

In delta connection,

$$R_{ab} = R_a(R_c.R_b) / (R_b+R_c)$$

$$R_{bc} = R_b(R_c.R_a) / (R_a+R_c)$$

$$R_{ca} = R_c(R_a.R_b) / (R_b+R_a)$$

Now for transformation,  $R_{ab} = R_{ab}$ ,  $R_{bc} = R_{bc}$ ,  $R_{ca} = R_{ca}$

$$(r_a + r_b) = R_a(R_c.R_b) / (R_b+R_c) \quad \text{---- 1}$$

$$(r_c + r_b) = R_b(R_c.R_a) / (R_a+R_c) \quad \text{---- 2}$$

$$(r_a + r_c) = R_c(R_a.R_b) / (R_b+R_a) \quad \text{---- 3}$$

### Delta to star transformation:

solve (1+3-2) we can find  $r_a$  in terms of  $R_a, R_b$  and  $R_c$ .

$$r_a = R_a R_c / (R_a + R_b + R_c)$$

Similarly, for  $r_b$  solve (1+2-3) and for  $r_c$  solve (2+3-1)

$$r_b = R_a R_b / (R_a + R_b + R_c)$$

$$r_c = R_b R_c / (R_a + R_b + R_c)$$

### Star to Delta Transformation:

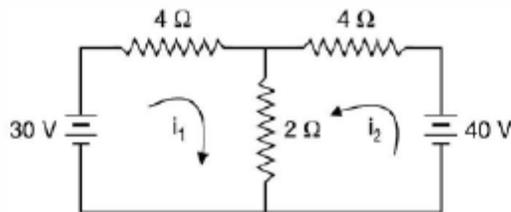
$$R_a = r_a r_b + r_b r_c + r_c r_a / r_c$$

$$R_b = r_a r_b + r_b r_c + r_c r_a / r_a$$

$$R_c = r_a r_b + r_b r_c + r_c r_a / r_b$$

## 2.2 MESH ANALYSIS:

Mesh analysis is a technique used to solve the complex networks consisting of more number of meshes. Mesh analysis is nothing but applying KVL to each and every loop in circuit and solving for mesh currents. By finding the mesh currents we can solve any require data of the network.



Let  $V_1 = 30\text{v}$ ,  $V_2 = 40\text{v}$ ,  $R_1 = 4\text{ ohms}$ ,  $R_2 = 2\text{ ohms}$  and  $R_3 = 4\text{ ohms}$

$i_1$ ,  $i_2$  are the mesh currents, here positive direction of currents are assumed, but in general we can assume current directions in any fashion and can solve.

Applying KVL to first loop we get,  $V_1 - i_1 R_1 - (i_1 + i_2) R_2$ .

$$V_1 = (R_1 + R_2) i_1 + i_2 R_2 \quad \text{---1}$$

Applying KVL to second loop we get,  $V_2 - i_2 R_3 - (i_1 + i_2) R_2$ .

$$V_2 = (R_1 + R_2) i_1 + i_2 R_3 \quad \text{---2}$$

Hence by solving eq. 1 and 2 we can get mesh currents  $i_1$  and  $i_2$ .

### 2.2.1 Mesh analysis by inspection method:

Inspection method is direct method using mesh currents can be find directly without applying KVL. Let us take same network as above , representing eq 1 and 2 in matrix form.

V1	=	R1	R1+R2	i1
V2		R1+R2	R3	i2

Generally we can write in matrix form as,

V1	=	R11	R12	i1
V2		R21	R22	i2

Where, V1 – sum of all the voltage sources in 1st mesh according current flow.

V2 – sum of all the voltage sources in 2<sup>nd</sup> mesh according current flow.

R11- self resistance of first loop, adding total resistance in 1<sup>st</sup> loop

R21= R12- mutual resistance between 1<sup>st</sup> and 2<sup>nd</sup> loop ,

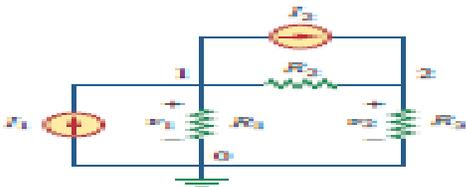
+ve if mesh currents are in same direction

-ve if mesh currents are in opposite direction

R22- self resistance of second loop, adding total resistance in 2<sup>nd</sup> loop

### 2.3 NODAL ANALYSIS :

Nodal analysis is a technique used to solve the complex networks consisting of more number of nodes. Node analysis is nothing but applying KCL to each and every node in circuit and solving for node voltages. By finding the node voltages we can solve any require data of the network.



For the above circuit current division takes place at two nodes 1 and 2.

Let , I3,I4,I5 are the currents flowing through R1,R2 and R3.

Applying KCL at node 1, I1 = I3+I4

$$= V_a / R1 + (V_a - V_b) / R2$$

$$= V_a(1/R_1 + 1/R_2) - V_b / R_2 \text{ ----1}$$

Applying KCL at node 2,  $I_2 + I_4 = I_5$

$$I_2 + (V_a - V_b) / R_2 = V_b / R_3$$

$$I_2 = -V_a / R_2 + V_b (1/R_3 + 1/R_2) \text{ ----2}$$

By solving above eq.1 and 2 we can get node voltages  $V_1$  and  $V_2$ .

### 2.3.1 Nodal analysis by inspection method:

Inspection method is direct method using node voltages can be find directly without applying KCL. Let us take same network as above , representing eq 1 and 2 in matrix form.

$I_1$	=	$(1/R_1 + 1/R_2)$	$-1/R_2$	$V_1$
$I_2$		$-1/R_2$	$(1/R_3 + 1/R_2)$	$V_2$

Generally we can write in matrix form as,

$I_1$	=	$G_{11}$	$G_{12}$	$V_1$
$I_2$		$G_{21}$	$G_{22}$	$V_2$

Where,  $I_1$  – sum of all the current sources in 1st node according current flow.

$I_2$  – sum of all the voltage sources in 2<sup>nd</sup> node according current flow.

$G_{11}$ - self conductance of first node, adding total conductance in 1<sup>st</sup> node

$G_{21} = G_{12}$ - mutual conductance between 1<sup>st</sup> and 2<sup>nd</sup> loop ,

Always -ve

$G_{22}$ - self conductance of second node, adding total conductance in 2<sup>nd</sup> node

### 2.4 CONVENTIONS:

- power delivered =  $V_s \cdot I_s$
- power lost =  $I^2 \cdot R$
- voltage is positive if flow is from negative to positive called as potential rise. ( $V_s$ )
- voltage is negative if flow is from positive to negative called as potential drop. ( $I \cdot R$ )

## 2.5 NETWORK TOPOLOGY:

Network topology is the one of the technique to solve electrical networks consisting of number of meshes or number of nodes, where it is difficult to apply mesh and nodal analysis.

Graph theory is the technique where all the elements of the network are represented by straight lines irrespective of their behaviour. Here matrix methods are used to solve complex networks. Before seeing the actual matrices, the knowledge of some of the definitions is very important. They are---

### 2.5.1 DEFINITIONS:

**Node :** An node is junction where two or more than two elements are connected.

**Degree of the node:** number of elements connected to the node is defined as degree of the node.

**Branch:** An branch is a element(s) connected between pair of nodes.

**Path:** It is traversal of signal between pair of nodes.

**Loop:** It is the path started from an node and ends at the same node.

**Graph:** An graph is formed when all the elements of the network are replaced by straight line irrespective of their behaviour.

**Oriented and non-oriented graph:** If the graph of the network is represented with directions in each and every branch then it is oriented, if atleast one branch of graph has no direction then it is non-oriented graph.

**Planar and non-planar graph:** if an graph can be on plane surface without cross over then system is planar and vice-versa is non-linear.

**Tree:** Tree is the sub-graph of the graph, which consists of same number of nodes as that of original graph without any closed path.

Branches of the tree are called as twigs. Number of possible twigs in an tree are  $(n - 1)$ .  
 $n$  – number of nodes

**Co-tree:** The set of branches which are removed to form tree are called as co-tree.

**Links:** Branches removed to form tree are called as links.

$$l = b - (n-1)$$

## 2.5.2 INCIDENCE MATRIX(A):

Incidence matrix is formed between number of nodes and number of branches. This matrix is useful easy understanding of network and any complex network can be easily feed into system for coding. Order of incidence matrix is (n\*b)

Procedure to incidence matrix:

$a_{ij} = 1$ , if jth branch is incidence to ith node and direction is away from node.

$a_{ij} = -1$ , if jth branch is incidence to ith node and direction is towards from node.

$a_{ij} = 0$ , if jth branch is not incidence to ith node .

Properties of incidence matrix:

1. Number of non zero entries of row indicates degree of the node.
2. The non zero entries of the coloumn represents branch connections.
3. If two coloumns has same entries then they are in parallel.

Reduced incidence matrix:

Reduced incidence matrix is formed by eliminating one of the row from incidence matrix generally ground node row is eliminating, which is representing by A!. Number of possible trees of for any graph are  $\det(A! A!T)$ .

Once we form the incidence matrix , we can write KCL equations any complex without applying KCL as follows,

$$A! \cdot I_b = 0$$

Where, A! - reduced incidence matrix

I<sub>b</sub> - branch current matrix( an coloumn matrix)

## 2.3 TIE-SET MATRIX:

Tie-set matrix is formed between link currents and branch currents. The order of tie-set matrix is (I<sub>l</sub>\*I<sub>b</sub>). it is represented by B. Tie-set is defined as a loop which consists of one link any number of branches. Hence total number of tie-set possible with above definition are number of links.

Procedure to form tie-set matrix:

$B_{ij} = 1$ , if current direction of  $j$ th branch coincides with direction of  $i$ th link.

$B_{ij} = -1$ , if current direction of  $j$ th branch opposes with direction of  $i$ th link.

$B_{ij} = 0$ , if  $j$ th branch has no relation with  $i$ th link.

Once we form tie-set matrix KVL equations of any complex network can be written as  $B.V_b = 0$

Where,  $B$  = tie-set matrix

$V_b$  = branch voltage matrix(column matrix)

From the knowledge of tie-set matrix we can calculate all the branch currents in terms of link currents, which is given as

$$I_b = B^T \cdot I_l$$

Where,  $I_b$  - branch current matrix( an column matrix)

$I_l$  - link current matrix( an column matrix)

$B^T$ - transpose of tie-set matrix

#### 2.5.4 CUT-SET MATRIX:

Cut-set matrix is formed between twig voltages and branch voltages. The order of cut-set matrix is  $((n-1)*b)$ . it is represented by  $C$ . Cut-set is defined as minimum set of branches by removing which graph is divided into two sub-graphs, where one of the part is an isolated node. Hence total number of cut-set possible with above definition are number of twigs. Generally cut-set direction is assumed in direction of branch, as cut-set consists of one branch any number of links.

Procedure to form tie-set matrix:

$c_{ij} = 1$ , if direction of  $j$ th branch coincides with direction of  $i$ th cut-set.

$c_{ij} = -1$ , if direction of  $j$ th branch opposes with direction of  $i$ th cut-set.

$c_{ij} = 0$ , if direction of  $j$ th branch is not in the  $i$ th cut-set.

Once we form cut-set matrix KCL equations of any complex network can be written as  $C.I_b = 0$

Where,  $C$ = cut-set matrix

$I_b$  = branch current matrix(column matrix)

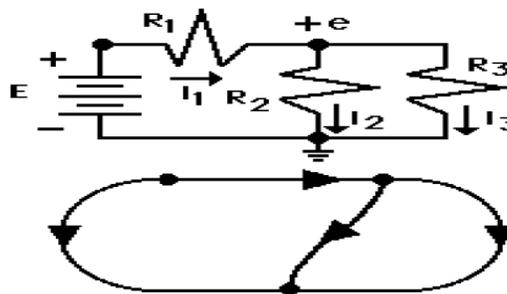
From the knowledge of cut-set matrix we can calculate all the branch voltages in terms of twig voltages, which is given as

$$V_t = C^T \cdot V_b$$

Where,  $V_b$  - branch voltage matrix( an coloumn matrix)

$V_t$  - twig voltage matrix( an coloumn matrix)

$C^T$ - transpose of cut-set matrix



Eg:

Determine all studied above for given circuit with its graph.

Nodes,  $n = 3$

Branches = 4

Twigs =  $3-1 = 2$

Links =  $4-3+1 = 2$

**Incidence matrix:**

<b>A</b>	=		<b>1</b>	<b>2</b>	<b>3</b>	<b>4</b>
		<b>a</b>	<b>1</b>	<b>1</b>	<b>0</b>	<b>0</b>
		<b>b</b>	<b>0</b>	<b>-1</b>	<b>1</b>	<b>1</b>
		<b>c</b>	<b>-1</b>	<b>0</b>	<b>-1</b>	<b>-1</b>

**Reduced Incidence matrix:**

<b>A!</b>	=		<b>1</b>	<b>2</b>	<b>3</b>	<b>4</b>
		<b>a</b>	<b>1</b>	<b>1</b>	<b>0</b>	<b>0</b>
		<b>b</b>	<b>0</b>	<b>-1</b>	<b>1</b>	<b>1</b>

**Tie-set matrix:**

As tree can be formed with two branches remaining two are links, let 2,4 are the links.

<b>B</b>	=		<b>i1</b>	<b>i2</b>	<b>i3</b>	<b>i4</b>
		<b>i2</b>	<b>-1</b>	<b>1</b>	<b>1</b>	<b>0</b>
		<b>i4</b>	<b>0</b>	<b>0</b>	<b>-1</b>	<b>1</b>

We can write all branch currents as,  $I_b = B^T \cdot I_l$

<b>i1</b>	=	<b>-1</b>	<b>0</b>	<b>i2</b>
<b>i2</b>		<b>1</b>	<b>0</b>	
<b>i3</b>		<b>1</b>	<b>-1</b>	<b>i4</b>
<b>i4</b>		<b>0</b>	<b>1</b>	

Hence ,  $i1 = -i2$   
 $i2 = i2$   
 $i3 = i2 - i4$   
 $i4 = i4$

**Cut-set matrix:**

Let the two cut-set are (1,2) and (2,3,4) as possible cut-sets are  $(n-1) = (3-1) = 2$ .

Here 1 and 3 are branches or twigs hence cutsets direction is same as these branch directions.

<b>C</b>	=		<b>1</b>	<b>2</b>	<b>3</b>	<b>4</b>
		<b>C(1,2)</b>	<b>1</b>	<b>-1</b>	<b>0</b>	<b>0</b>
		<b>C(2,3,4)</b>	<b>0</b>	<b>-1</b>	<b>1</b>	<b>1</b>

We can write all branch voltages as,  $V_b = C^T \cdot V_t$

V1	=	1	0	V1
V2		-1	-1	
V3		0	1	V3
V4		0	1	

Hence,  $V1 = V1$

$V2 = -V1 - V3$

$V3 = V3$

$V4 = V3$

## 2.6 DUAL AND DUALITY:

Some times for easy simplification of network we may need dual network of original network. Dual network is formed by using dual parameters.

Dual parameters:

Series	Parallel
Parallel	Series
Voltage	Current
Current	Voltage
Resistance	Conductance
Inductance	capacitance
Capacitance	Inductance
Open	Short
Short	open

Procedure to draw dual network for original network:

1. Firstly assume node in each an every loop and node outside the circuit.
2. Now replace the element which purely belongs to respective loop with its dual element between node assumed in that loop and node outside loop.
3. Now replace the element which belongs two loops with its dual element between node assumed in that loop and node assumed in other loop.

\*\*\* Even we draw the dual network for original network the behaviour of network willnot change.

## **UNIT – III**

# **SINGLE PHASE AC CIRCUITS**

### 3.1 INTRODUCTION:

The alternating quantity is one whose value varies with time. This alternating quantity may be periodic and non-periodic. Periodic quantity are one whose value will be repeated for every specified interval . Generally to represent alternating voltage or current we prefer sinusoidal wave form , because below listed properties—

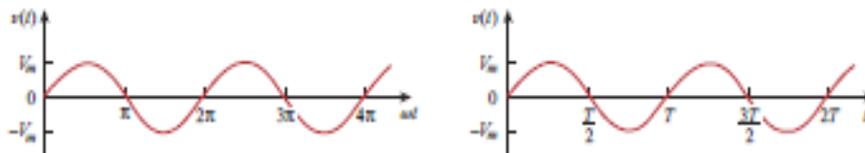
1. Derivative of sine is an sine function only.
2. Integral of sine is an sine function only.
3. It is easy to generate sine function using generators.
4. Most of the 2<sup>nd</sup> order system response is always sinusoidal.

### 3.2 Alternating quantity:

As said above an alternating voltage or current can be represented with sine wave. Sine wave can be defined with degree or radians as reference.

At, 0 degrees --- 0  
90 degrees --- maximum  
180 degrees --- 0  
270 degrees --- maximum  
360 degrees --- 0

i.e value of sine function varies with time, firstly increases from zero and reaches maximum and again falls to zero, there after tends to increase in opposite direction and reaches maximum value and falls to zero. This the variation of sine in 1<sup>st</sup> cycle is called as positive half cycle and other negative half cycle.(i.e during +ve half cycle direction is required one and during 2<sup>nd</sup> half cycle direction actual required direction.). Therefore one positive and negative cycle combinely forms one complete cycle.



Sine equation , voltage ,  $V(t) = V_m \sin wt$ .

Where,  $V_m$  = peak value or maximum value  
 $W$  = angular frequency.

### 3.3 Definitions:

**Peak to peak value:** It is total value from positive peak to the negative peak.( $2V_m$ )

**Instantaneous value:** It is the magnitude of wave form at any specified time.  $V(t)$

**Average value :** It is ratio of area covered by wave form to its length.( $V_d$ )

$$V_d = (1/T) \int V(t) dt$$

$$V_d = (1 / 2\pi) \int V_m \sin \omega t . dt$$

$$= - V_m / 2\pi . \cos \omega t \text{---with limits of } 2\pi \text{ and } 0$$

$$= 0. \text{( i.e average value of sine wave over a full cycle is zero)}$$

Hence it is defined for half cycle.

$$V_d = (1 / \pi) \int V_m \sin \omega t . dt$$

$$= - V_m / \pi . \cos \omega t \text{---with limits of } \pi \text{ and } 0$$

$$= 2V_m / \pi$$

**RMS value:**

It is the root mean square value of the function, which given as

$$V_{rms} = \sqrt{[(1/T) \int V(t)^2 dt]}$$

$$= \sqrt{[(1/2\pi) \int V_m^2 (1 - \cos 2\omega t)/2] dt}$$

$$= \sqrt{[(1/2\pi) . V_m^2 ( \omega t - \sin 2\omega t / 2\omega t)/2]}$$

$$= V_m / \sqrt{2} = \text{effective value.}$$

**Peak factor:**

It is the ratio of peak value to the rms value.

$$P_p = V_p / V_{rms} = \sqrt{2}$$

**Form factor:**

It is the ratio of average value to the rms value.

$$F_p = V_d / V_{rms} = 2\sqrt{2} / \pi = 1.11$$

Eg: Find the peak, peak to peak, average, rms, peak factor and form factor of given current function ,  $i(t) = 5 \sin wt$ .

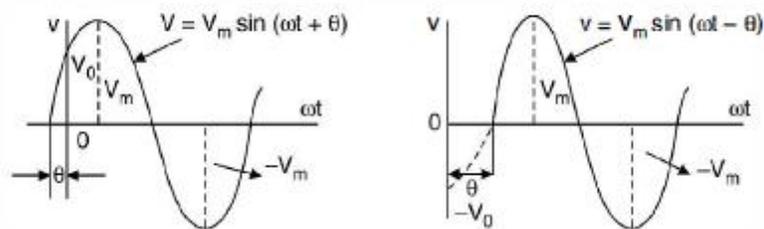
### 3.4 Phase and phase difference:

Phase of the sine indicates starting phase of the sine wave. i.e

Let ,  $V(t) = V_m \sin wt$ , here we can say that phase is zero as function starts from origin.

$V(t) = V_m \sin(wt - \theta)$ , here we can say that phase of function is  $\theta$  degrees to right shift.

$V(t) = V_m \sin(wt + \theta)$ , here we can say that phase of function is  $\theta$  degrees to left shift.



Phase difference is the difference of phase between two wave forms taking one as reference.

Eg: If wave form A is  $V_m \sin (wt+15)$ , B is  $V_m \sin (wt - 30)$  and C is  $V_m \sin (wt + 45)$ . Determine the phase difference between every pair if wave forms.

When A and B are compared , phase difference is 45 degrees.

When C and B are compared , phase difference is 75 degrees.

When A and C are compared , phase difference is 30 degrees.

#### 3.4.1 Phasor diagram:

Phasor diagram is the pictorial representation of sine wave. Here magnitude and phase of the wave function are represented in four quadrant axis. We assume positive phases in anti-clock wise direction and negative phases in clock wise direction. From the phasor diagram we can easily identify the phase difference between different wave forms. We can also identify whether function is right shift or left shift.

### 3.5 Phase relations of network parameters:

#### Resistor:

Let us consider resistor allowing alternating current  $i(t)$ . then the voltage drop across resistor is given as,

$$\text{If, } V(t) = V_m \sin \omega t$$

$$V(t) = i(t) \cdot R$$

$$i(t) = V(t) / R$$

$$= V_m \sin \omega t / R$$

$$i(t) = I_m \sin \omega t.$$

The ratio of  $V(t) / i(t) = Z =$  impedance offered by resistor.(ohms).

$$Z = V_m \sin \omega t / I_m \sin \omega t.$$

$$= V_m / I_m$$

Hence we can say that  $V(t)$  and  $i(t)$  in resistor element are in phase.

#### Inductor:

Let us consider an coil of  $N$  turns allowing current  $i(t)$ . ( $I_m \sin \omega t$ )

Hence emf induced in the coil is ,

$$V(t) = L di(t) / dt$$

$$= L d(I_m \sin \omega t) / dt$$

$$= L \omega I_m \cos \omega t$$

$$= V_m \cos \omega t = V_m \sin(\omega t + 90).$$

Where,  $V_m = L \omega I_m = I_m \cdot X_L$

$X_L$  = reactance offered by coil.

Impedance offered by coil is ,  $Z = V(t) / i(t)$

$$= V_m \sin(\omega t + 90) / I_m \sin \omega t$$

The function  $V_m \sin \omega t = V_m \angle 0$ .

$$Z = V_m \angle 90 / I_m \angle 0$$

$$Z = V_m \angle 90 / I_m \text{ Type equation here.}$$

$$= j \omega L = j X_L \quad (j = \angle 90)$$

As there is left shift in  $V(t)$ , we can say that  $i(t)$  lags  $V(t)$  by 90 degrees.

### Capacitor:

Let us consider an capacitor allowing current  $i(t)$ . ( $I_m \sin \omega t$ )

Hence voltage across it is ,

$$\begin{aligned} V(t) &= 1 / C \int i(t) dt \\ &= 1 / C \int I_m \sin \omega t dt \\ &= -\cos \omega t \cdot I_m / \omega C \end{aligned}$$

$$= V_m \sin(\omega t - 90).$$

Where,  $V_m = I_m / \omega C = I_m \cdot X_C$

$X_C$  = reactance offered by capacitor

Impedance offered by capacitor is ,  $Z = V(t) / i(t)$

$$= V_m \sin(\omega t - 90) / I_m \sin \omega t$$

The function  $V_m \sin \omega t = V_m \angle 0$ .

$$Z = V_m \angle -90^\circ / I_m \angle 0^\circ$$

$$Z = V_m \angle -90^\circ / I_m \text{ Type equation here.}$$

$$= -j \omega L = -j X_L \quad (j = \angle 90^\circ)$$

As there is right shift in  $V(t)$ , we can say that  $i(t)$  leads  $V(t)$  by 90 degrees.

### 3.6 Power in Ac circuits:

In the case of DC circuits power is given as product of voltage and current in that element.

$$P = V \cdot I \text{ (W)}$$

$$\text{Let } V(t) = V_m \sin \omega t$$

$$i(t) = I_m \sin(\omega t + 90^\circ)$$

$$\text{instantaneous power, } P(t) = V(t) \cdot i(t)$$

$$= V_m \sin \omega t \cdot I_m \sin(\omega t + \Phi)$$

$$= V_m \cdot I_m \sin \omega t \sin(\omega t + \Phi)$$

$$= V_m \cdot I_m \cdot 2 \cdot \sin \omega t \sin(\omega t + \Phi)$$

$$\frac{\text{-----}}{2}$$

$$= V_m \cdot I_m \cdot 2 \cdot \sin \omega t \sin(\omega t + \Phi)$$

$$\frac{\text{-----}}{\sqrt{2} \cdot \sqrt{2}}$$

$$= V_m \cdot I_m [\cos \Phi - \cos(2\omega t + \Phi)]$$

$$\frac{\text{-----}}{\sqrt{2} \cdot \sqrt{2}}$$

Average power ,  $P_{av} = 1/ 2\pi \int p(t) dt$ .

$$= \frac{1/ 2\pi \int V_m I_m [ \cos \Phi - \cos( 2\omega t + \Phi) ] dt}{\sqrt{2} \cdot \sqrt{2}}$$

As average value over full cycle is equal to zero, hence second term can be neglected.

$$P_{av} = \frac{1/ 2\pi \int V_m I_m [ \cos \Phi ] dt}{\sqrt{2} \cdot \sqrt{2}}$$

$$= \frac{V_{rms} I_{rms} \cos \Phi [wt] \text{ ----- with limits } 2\pi \text{ and } 0}{2\pi}$$

$P_{av} = V_{rms} \cdot I_{rms} \cos \Phi \cdot (W) = \text{true power} = \text{active power}.$

$\cos \Phi = P_{av} / V_{rms} \cdot I_{rms} = \text{defined as power factor of the circuit}.$

$$\cos \Phi = P_{av} / P_a$$

$$= \text{true power} / \text{apparent power}$$

$$= \text{actual power utilized by load} / \text{total generated power}.$$

$$P_a = \text{apparent power} = V_{rms} \cdot I_{rms} = V \cdot A$$

Let us consider commercial inductor,

$$Z = R + jXL$$

Where,  $Z = \text{impedance of the coil}$

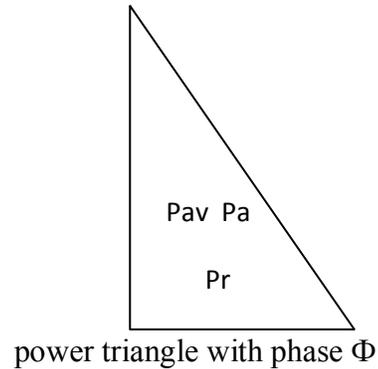
$R = \text{internal resistance of the coil}$

$X_L$  = reactance offered by the coil.

$$I(t) Z = I(t) R + I(t) jX_L$$

$$I^2 Z = I^2 R + j I^2 X_L$$

$$P_a = P_{av} + j P_r$$



$$P_{av} = P_a \cos \Phi = V_{rms}.I_{rms} \cos \Phi = \text{active power} = W$$

$$P_r = P_a \sin \Phi = V_{rms}.I_{rms} \sin \Phi = \text{reactive power} = VAR$$

Let us consider commercial capacitor,

$$Z = R - jX_C$$

Where,  $Z$  = impedance of the capacitor

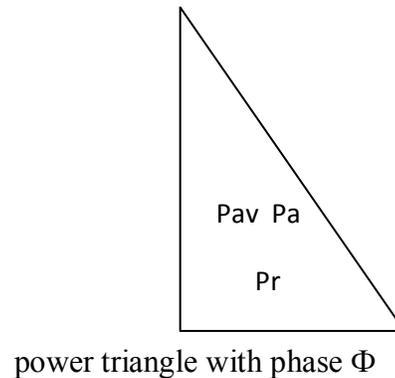
$R$  = internal resistance of the capacitor

$X_C$  = reactance offered by the capacitor.

$$I(t) Z = I(t) R - I(t) jX_C$$

$$I^2 Z = I^2 R - j I^2 X_C$$

$$P_a = P_{av} - j P_r$$



$$P_{av} = P_a \cos \Phi = V_{rms}.I_{rms} \cos \Phi = \text{active power} = W$$

$$P_r = P_a \sin \Phi = V_{rms}.I_{rms} \sin \Phi = \text{reactive power} = VAR$$

### 3.7 Complex power:

Complex power is represented with S.

$$S = V(t) \cdot i(t)^*$$

$$= P + jQ \text{ or } P - jQ$$

Where, P = active power

Q = reactive power

Here only useful power is true power where as net reactive power over an cycle will be zero.

### 3.8 Complex numbers:

Complex numbers can be represented in two ways, either rectangle form or polar form

Rectangular form =  $a + j b$

Polar form =  $\sqrt{a^2 + b^2} \angle \tan^{-1}(b/a)$

Here j operator plays major role in complex number, which is define unit vector rotating in anti-clock wise direction with phase 90.

$$j = 1 \angle 90 = \sqrt{-1}$$

$$j^2 = -1$$

$$j^3 = -\sqrt{-1}$$

## **UNIT – IV**

# **RESONANCE AND MAGNETIC CIRCUITS**

## 4.1 MAGNETIC CIRCUITS

Let us consider an coil allowing current of  $IA$  which develops magnetic lines of force forming north and south poles , the flow of magnetic lines from north pole to south pole. If coil is wounded on some core allowing current  $IA$  develops flux  $\Phi$  and this flux follows the path of core to form magnetic circuit.

### 4.2 Definitions:

Magnetic flux density: Flux developed per unit area. ( $\Phi / A$ ). Represented with  $B$ .

Whose units are webers/mt<sup>2</sup> or tesla.

MMF( Magneto motive force): It is the measure of ability of amount of flux can be developed in the coil.( $J$ ), which is given as product of number of turns and current flowing through coil.

$$J = N.I \text{ (A-turns)}$$

Field intensity: It is defined as mmf per unit length.( $H$ )

$$H = \text{mmf} / l \text{ ( A-turns / mt)}$$

Reluctance: It is the property of core which opposes magnetic flux. Generally cores of two types ,they are air and iron core. When compare to iron core air core has more reluctance Property.

(or)

Reluctance is ratio of mmf to the flux.(  $J / \Phi$ )

$$R = (l / \mu.A) .$$

Where,  $l$  – mean length of magnetic circuit.

$A$  – area of cross of core.

$\mu$  - permeability of the core.

- $\mu_0. \mu_r$
- absolute permeability( $\mu_0$ )
- relative permeability( $\mu_r$ )—varies for different types of cores.

Hence mmf is also given as , $J = R. \Phi$

Fringing and leakage effect:

Let us consider ring core with small air gap. When flux developed in core, during flow of flux if there is a sudden change in core whose values are largely differ , flux suddenly bulges out which is called as fringing.

Generally core laminated and these lamination may consists of some weak points and flux leaked through these weak points is called as leakage flux.

#### **4.3 Series magnetic circuit:**

Let us consider an coil of  $N$  turns wounded on ring core. When some current  $I$  A is allowed through coil flux  $\Phi$  is developed in it.

Let, mmf required to develop  $\Phi$  is  $J$

$R$  is reluctance of core.

$N$ - number of turns.

$I$ - Current through coil.

Hence , mmf,  $J = N.I$

Drop in core is  $= \Phi.R$

$$J = \Phi.R = N.I$$

Therefore flux developed in coil is given as,  $\Phi = N.I / R$

#### **4.4 Composite magnetic circuit:**

Let us consider ring core which comprises of three different materials with different lengths and areas. An coil of  $N$  turns is wounded on such core as described above, allowing current  $I$  A.

Let ,  $\Phi_1$  = flux developed in the first part of core

$R_1$  = reluctance of first part of the core

$l_1$  = length of first part of the core

$A_1$  = area of first part of core

$J_1$  = mmf drop in first part of core

$\Phi_2$  = flux developed in the 2nd part of core

$R_2$  = reluctance of 2nd part of the core

$l_2$  = length of 2nd part of the core

$A_2$  = area of 2nd part of core

$J_2$  = mmf drop in 2nd part of core

$\Phi_3$  = flux developed in the 3<sup>rd</sup> part of core

$R_3$  = reluctance of 3<sup>rd</sup> part of the core

$l_3$  = length of 3<sup>rd</sup> part of the core

$A_3$  = area of 3<sup>rd</sup> part of core

$J_3$  mmf drop in 3<sup>rd</sup> part of core

Hence total mmf required,  $J = J_1 + J_2 + J_3$   
 $= \Phi_1.R_1 + \Phi_2.R_2 + \Phi_3.R_3 = N.I$

Total flux developed is  $= NI / (R_1 + R_2 + R_3)$

Where ,  $R_1 = (l_1 / \mu_1.A_1)$

$R_2 = (l_2 / \mu_2.A_2)$

$R_3 = (l_3 / \mu_3.A_3)$

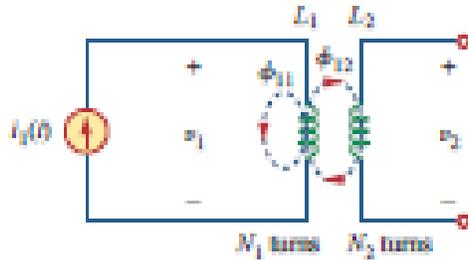
#### 4.5 Coupled circuits:

When two coils are brought together as close as possible then they form coupled coils.

Here when current ( $i_1$ ) is allowed through first coil then magnetic flux  $\Phi_1$  is developed in it, as other coil brought to close proximity some of  $\Phi_1$  links with second coil called as  $\Phi_{m1}$  their by inducing voltage in it and when we close the second coil current flows in it ( $i_2$ ). This current  $i_2$  develops  $\Phi_2$  in it and some of  $\Phi_2$  links with 1<sup>st</sup> coil called as  $\Phi_{m2}$ . If the two coils are of same dimensions  $\Phi_{m1} = \Phi_{m2} = \Phi_m$ .

Here we define two inductances self inductance of coils  $L_1$  and  $L_2$ , mutual inductance between the coils  $M_{12} = M_{21} = M$ . Now we can say that total emf induced in coil is the combination of self and mutually induced emf.

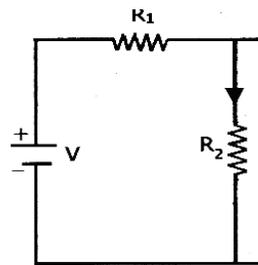
Emf in 1<sup>st</sup> coil ,  $v_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$   
 Emf in 2<sup>nd</sup> coil ,  $v_2 = L_2 \frac{di_2}{dt} + M \frac{di_1}{dt}$



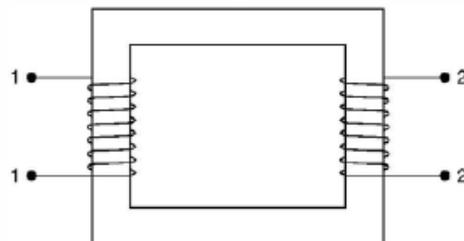
#### 4.2.1 Types of coupled coils:

Coupled coils are of three types, they are

1. Conductively coupled: Here an voltage is fed to the potential divider circuit  
 Called as conductively coupled

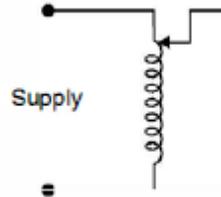


2. Inductively coupled: where there is no electrical connection, i.e electrically  
 Isolated but magnetically coupled.



Eg: Transformer

3. Conductively and inductively coupled: an best device which can be as conductively and inductively coupled is auto-transformer.



#### 4.5.2 Dot Convention:

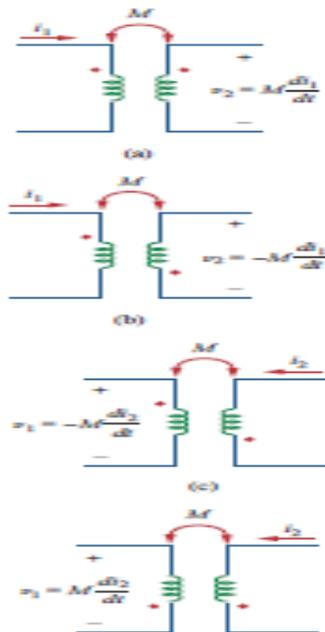
Dot convention is the method used to find whether mutually induced emf is positive or negative. Dot convention method is based on right hand thumb rule. Right hand thumb rule states that if thumb indicates direction of current then remaining folded fingers indicates how the coil is wound.

When we represent coupled coils, they may be indicated with dots. Dot convention says that,

If both the currents enter the dot then mutually induced emf is positive.

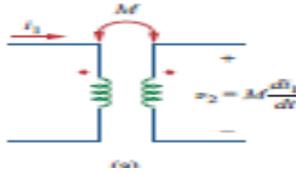
If both the currents leaving the dot then mutually induced emf is positive.

If one of the current enters the dot and the other leaves the dot then mutually induced emf is negative.



### 4.5.3 co-efficient of coupling:

Let us consider coupled coil as shown below



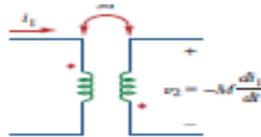
$$\begin{aligned} \text{Here, } v_1 &= L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \\ v_2 &= L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \end{aligned}$$

total energy stored is,  $w = \int v_1 \cdot i_1 dt + \int v_2 \cdot i_2 dt$

$$= \int (L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}) \cdot i_1 dt + \int i_2 d(L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}) dt$$

$$w = (1/2 L_1 i_1^2) + (1/2 L_2 i_2^2) + M i_1 i_2$$

similarly,



Total energy stored is,  $w = (1/2 L_1 i_1^2) + (1/2 L_2 i_2^2) - M i_1 i_2$

$$\frac{1}{2} (i_1 \sqrt{L_1} - i_2 \sqrt{L_2})^2 + i_1 i_2 (\sqrt{L_1 L_2} - M) \geq 0$$

To say energy is positive,  $\sqrt{(L_1 \cdot L_2)} - M \geq 0$ .

By removing the proportionality,  $K = M / \sqrt{(L_1 \cdot L_2)}$ .

Here K is defined as co-efficient of coupling maximum value of 1. If K=1 then coils are said to be perfectly coupled i.e maximum mutual flux linkage takes place.

## 4.6 RESONANCE:

If an electrical circuit offers impedance which is purely resistive then it is said to be under resonance and frequency of the circuit at which it happens is called as resonant frequency. While studying the resonance of electrical circuits we understand terms like resonant frequency, bandwidth, cut-off frequencies and quality factor.

### **Resonant frequency:**

It is the frequency at which maximum response occurs or net impedance is purely resistive or minimum impedance is offered by circuit. ( $f_r$ )

### **Bandwidth:**

It is the range of frequencies within which signal can be easily transmitted without any overlap of other signals. It is also given as difference between higher cut-off frequency and lower cut-off frequency. ( $B_w = f_h - f_l$ )

### **Cut-off frequencies:**

It is the frequency at which response of the circuit is the 70.7% of maximum value or 0.707 of maximum value. This can happen at two frequencies called as lower cut-off frequencies  $< f_r$  and higher cut-off frequencies  $> f_r$ .

### **Quality factor:**

Quality factor is the measurement of quality of the energy storing elements, which in turn indicates life time of energy storing elements.

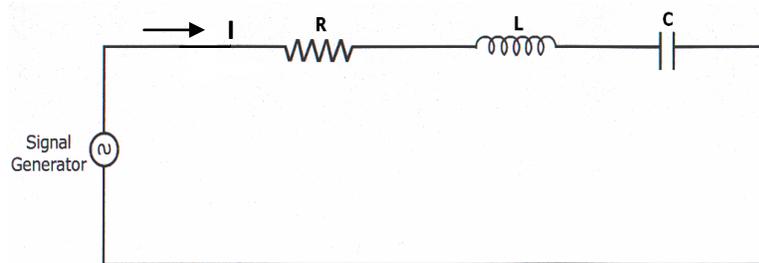
$$Q = \frac{2\pi * \text{energy stored in the element}}{\text{Energy dissipated in one cycle.}}$$

#### 4.6.1 Types of resonance:

Depending on types of circuit resonance is defined. The are

- 4 Series resonance:** series is related to series RLC circuit. In an series RLC circuit resonance occurs when voltage across L and C are same in magnitude and 180 degrees out of phase.
- 5 Parallel resonance:** series is related to Parallel RLC circuit. In an Parallel RLC circuit resonance occurs when current flowing through L and C are same in magnitude and 180 degrees out of phase.

#### 4.6.2 Series Resonance:



Let us consider series RLC circuit as shown,

$$\text{Here, } Z = R + j(X_L - X_C)$$

$$\text{Where, } X_L = 2\pi fL$$

$$X_C = 1 / 2\pi fC$$

To say that circuit is under resonance ,  $Z = R$

This happens only when,  $X_L = X_C$  i.e imaginary part of total impedance is zero.  
(  $X_L - X_C = 0$  )

$$X_L = X_C$$

$$2\pi fL = 1 / 2\pi fC$$

$$\omega L = 1 / \omega C \quad (\omega = 2\pi f, \text{ angular frequency rad/sec})$$

$$\omega^2 = 1/\sqrt{LC}$$

$f_r = 1/2\pi\sqrt{LC}$  --- resonant frequency.

### IMPEDANCE CURVE:

We know that,  $Z = R + j(XL - XC)$

$$Z = \sqrt{R^2 + (XL - XC)^2}$$

**For the lower frequencies** ,  $XC > XL$  the total impedance is

$$Z = \sqrt{R^2 + (XC - XL)^2}$$

And current through circuit is ,  $I = V / \sqrt{R^2 + (XC - XL)^2}$

Here we can say that at lower frequencies  $Z$  is very high as  $XC$  is infinitely high and current is very low, but as frequency increases towards  $f_r$   $X_c$  value decreases and  $(XC - XL)$  decreases and  $Z$  decreases their by current increases.

**At resonant frequency**,  $XL = XC$

$$Z = R \text{ (minimum value)}$$

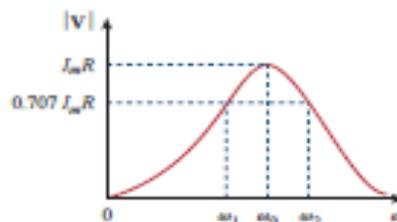
And current is ,  $I = V / R = \text{maximum current}$

**For the higher frequencies** ,  $XL > XC$  the total impedance is

$$Z = \sqrt{R^2 + (XL - XC)^2}$$

And current through circuit is ,  $I = V / \sqrt{R^2 + (XL - XC)^2}$

Here we can say that at higher frequencies  $Z$  is decreases as  $XL$  increases and current is also decreases, as frequency increases towards very high frequencies  $XL$  value increases and  $(XL - XC)$  increases and  $Z$  increases their by current decreases.



Here for frequencies  $< f_r$  circuit is said to be dominantly capacitive and for frequencies  $> f_r$  circuit is said to be dominantly inductive.

### **BANDWIDTH :**

Let  $f_1, f_2$  --- lower and higher cut-off frequencies

$$\text{At } f_1, I = V / \sqrt{2R}$$

$$\text{And also at } f_2, I = V / \sqrt{2R}$$

This is possible only when ,

$$\text{At } f_1, 1/w_1 C - w_1 L = R \text{ ----1}$$

$$f_2, w_2 L - 1/w_2 C = R \text{ ----2}$$

equate 1 and 2

$$1/w_1 C - w_1 L = w_2 L - 1/w_2 C$$

$$1/w_1 C - w_1 L = w_2 L - 1/w_2 C$$

$$w_1 w_2 = 1/LC$$

$$w_1 w_2 = w_r^2$$

now add two equations,

$$1/w_1 C - w_1 L + w_2 L - 1/w_2 C = 2R$$

$$(w_2 - w_1)L + (w_2 - w_1)/w_1 w_2 C = 2R$$

$$\text{By sloving above equation, } f_2 - f_1 = R / 2\pi L$$

$$\text{Lower cut off frequency } (f_1) = f_r - R/4\pi L$$

$$\text{Upper cut off frequency } (f_2) = f_r + R/4\pi L$$

**Quality factor:** For inductor.

$$Q = \frac{2\pi * \text{energy stored in the element}}{\text{Energy dissipated in one cycle.}}$$

$$Q = \frac{2\pi * \frac{1}{2} LI^2}{I^2 \cdot R \cdot t}$$

$$Q = \frac{2\pi * \frac{1}{2} LI^2}{I^2 \cdot R \cdot 1/f}$$

$$Q = 2\pi L / R = X_L / R$$

For capacitor.

$$Q = \frac{2\pi * \text{energy stored in the element}}{\text{Energy dissipated in one cycle.}}$$

$$Q = \frac{2\pi * \frac{1}{2} CV^2}{I^2 \cdot R \cdot t}$$

$$Q = \frac{2\pi * \frac{1}{2} CV^2}{(V/\sqrt{2R})^2 \cdot R \cdot 1/f}$$

$$Q = 1 / 2\pi fC R = X_C / R$$

### MAGNIFICATION:

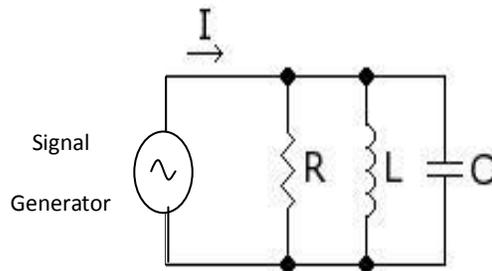
Magnification is defined ratio voltage across energy storing elements and input voltage under resonance.

$$V_L / V_i = I_XL / IR = XL / R = Q$$

$$V_C / V_i = I_XC / IR = XC / R = Q$$

To say that life of the circuit is high the magnification must be high.

#### 4.6.3 Parallel Resonance:



Let us consider parallel RLC circuit as shown,

$$\text{Here, } Y = 1/R + j(1/XL - 1/XC) = G + j(BL - BC)$$

$$\text{Where, } BL = 1 / 2\pi fL$$

$$BC = 2\pi fC$$

To say that circuit is under resonance ,  $Y = G$

This happens only when,  $BL = BC$  i.e imaginary part of total impedance is zero.  
(  $BL - BC = 0$  )

$$BL = BC$$

$$1 / 2\pi fL = 2\pi fC$$

$$1 / \omega L = \omega C \quad (\omega = 2\pi f, \text{ angular frequency rad/sec})$$

$$\omega^2 = 1 / \sqrt{LC}$$

$$f_r = 1 / 2\pi\sqrt{LC} \text{--- resonant frequency.}$$

### ADMITTANCE CURVE:

We know that,  $Y = G + j(BL - BC)$

$$Y = \sqrt{G^2 + (BL - BC)^2}$$

**For the lower frequencies**,  $BL > BC$  the total admittance is

$$Y = \sqrt{G^2 + (BL - BC)^2}$$

And current through circuit is,  $V = I / \sqrt{G^2 + (BL - BC)^2}$

Here we can say that at lower frequencies  $Y$  is very high as  $BL$  is infinitely high and voltage is very low, but as frequency increases towards  $f_r$   $BL$  value decreases and  $(BL - BC)$  decreases and  $Y$  decreases their by voltage increases.

**At resonant frequency**,  $BL = BC$

$$Y = 1 / R \text{ (minimum value)}$$

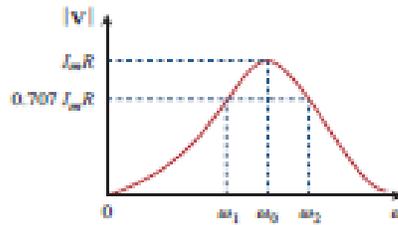
And voltage is,  $V = I / G = \text{maximum current}$

**For the higher frequencies**,  $BC > BL$  the total admittance is

$$Y = \sqrt{G^2 + (BC - BL)^2}$$

And current through circuit is,  $V = I / \sqrt{G^2 + (BC - BL)^2}$

Here we can say that at higher frequencies  $Y$  is decreases as  $BC$  increases and voltage is also decreases, as frequency increases towards very high frequencies  $BC$  value increases and  $(BC - BL)$  increases and  $Y$  increases their by voltage decreases.



Here for frequencies  $< f_r$  circuit is said to be dominantly inductive and for frequencies  $> f_r$  circuit is said to be dominantly capacitive.

### BANDWIDTH :

Let  $f_1, f_2$  --- lower and higher cut-off frequencies

$$\text{At } f_1, V = I / \sqrt{2G}$$

$$\text{And also at } f_2, V = I / \sqrt{2G}$$

This is possible only when ,

$$\text{At } f_1, \omega_1 C - 1/\omega_1 L = G \text{ ----1}$$

$$f_2, 1/\omega_2 L - \omega_2 C = G \text{ ----2}$$

equate 1 and 2

$$\omega_1 C - 1/\omega_1 L = 1/\omega_2 L - \omega_2 C$$

$$1/\omega_1 C - \omega_1 L = \omega_2 L - 1/\omega_2 C$$

$$\omega_1 \omega_2 = 1/LC$$

$$\omega_1 \omega_2 = \omega_r^2$$

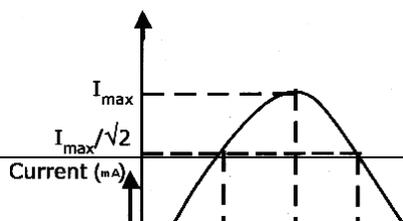
now add two equations,

$$\omega_1 C - 1/\omega_1 L + 1/\omega_2 L - \omega_2 C = 2G$$

$$\text{By sloving above equation, } f_2 - f_1 = 1/2\pi RC$$

$$\text{Lower cut off frequency } (f_1) = f_r - 1/4\pi RC$$

### SERIES RESONANCE



Upper cut off frequency  $(f_2) = f_r + 1/4 \omega RC$

**Quality factor:** For inductor.

$$Q = \frac{2\pi * \text{energy stored in the element}}{\text{Energy dissipated in one cycle.}}$$

$$Q = \frac{2\pi * \frac{1}{2} L(V/XL)^2}{(V / \sqrt{2R})^2 \cdot t}$$

$$Q = \frac{2\pi * \frac{1}{2} LI^2}{I^2 \cdot R \cdot 1/f}$$

$$Q = R / XL$$

For capacitor.

$$Q = \frac{2\pi * \text{energy stored in the element}}{\text{Energy dissipated in one cycle.}}$$

$$Q = \frac{2\pi * \frac{1}{2} CV^2}{I^2 \cdot R \cdot t}$$

$$Q = \frac{2\pi * \frac{1}{2} CV^2}{(V/\sqrt{2R})^2 \cdot R \cdot 1/f}$$

$$Q = R / BC = XC \cdot R$$

**MAGNIFICATION:**

Magnification is defined ratio voltage across energy storing elements and input voltage under resonance.

$$I_L / I = V / BL / V / R = R / BL$$

$$I_C / I_i = V / BC / V / R = R / BC = Q$$

To say that life of the circuit is high the magnification must be high.

**UNIT – V**

**NETWORK THEOREMS (DC AND AC)**

## UNIT-V

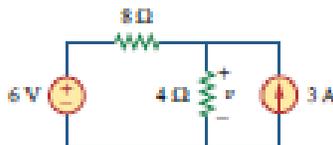
### 5.1 INTRODUCTION:

Network theorems are also can be termed as network reduction techniques. Each and every theorem got its importance of solving network. Let us see some important theorems with DC and AC excitation with detailed procedures.

### 5.2 SUPER-POSITION THEOREM:

**DC:** “ In an any linear , bi-lateral network consisting number of sources , response in any element(resistor) is given as sum of the individual Responses due to individual sources, while other sources are non-operative”

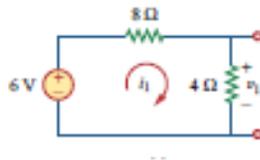
**AC:** “ In an any linear , bi-lateral network consisting number of sources , response in any element(impedance) is given as sum of the individual Responses due to individual sources, while other sources are non-operative”



Eg:

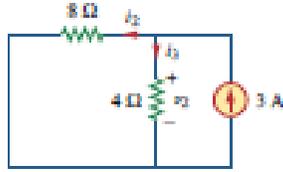
Let  $V = 6\text{v}$ ,  $I = 3\text{A}$ ,  $R_1 = 8\text{ ohms}$  and  $R_2 = 4\text{ ohms}$

Let us find current through 4 ohms using V source , while I is zero. then equivalent circuit is



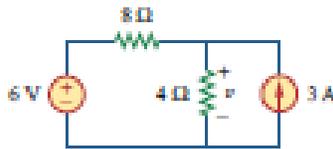
Let  $i_1$  is the current through 4 ohms,  $i_1 = V / (R_1+R_2)$

Let us find current through 4 ohms using I source , while V is zero. then equivalent circuit is



Let  $i_2$  is the current through 4 ohms,  $i_2 = I \cdot R_1 / (R_1+R_2)$

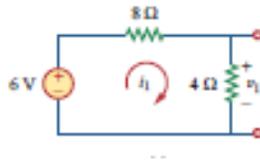
Hence total current through 4 ohms is =  $I_1+I_2$  ( as both currents are in same direction or otherwise  $I_1-I_2$ )



**Eg:**

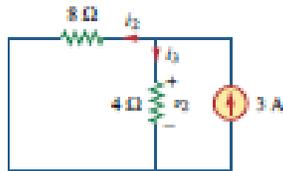
Let  $V = 6v$ ,  $I = 3A$ ,  $Z_1 = 8$  ohms and  $Z_2 = 4$  ohms

Let us find current through 4 ohms using  $V$  source , while  $I$  is zero.then equivalent circuit is



Let  $i_1$  is the current through 4 ohms,  $i_1 = V / (Z_1+Z_2)$

Let us find current through 4 ohms using  $I$  source , while  $V$  is zero.then equivalent circuit is

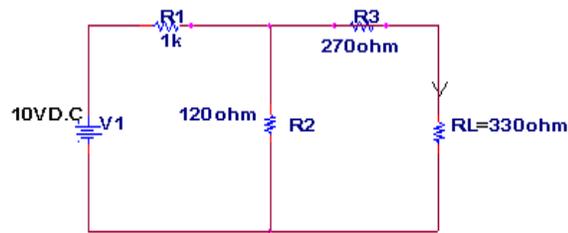


Let  $i_2$  is the current through 4 ohms,  $i_2 = I \cdot Z_1 / (Z_1+Z_2)$

Hence total current through 4 ohms is =  $I_1+I_2$  ( as both currents are in same direction or otherwise  $I_1-I_2$ ).

### 5.3 RECIPROCITY THEOREM:

DC & AC: “ In any linear bi-lateral network ratio of voltage in one mesh to current in other mesh is same even if their positions are inter-changed”.



Eg:

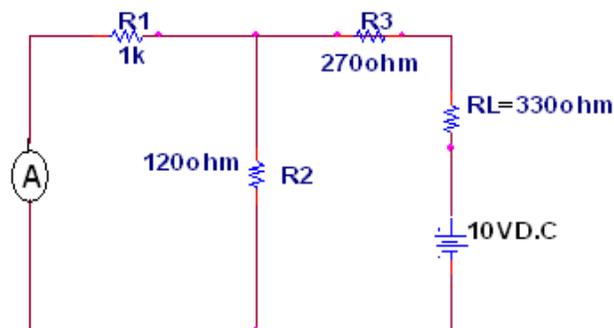
Find the total resistance of the circuit,  $R_t = R_1 + [R_2(R_3+R_L)] / R_2+R_3+R_L$ .

Hence source current,  $I = V_1 / R_t$ .

Current through  $R_L$  is  $I_1 = I \cdot R_2 / (R_2+R_3+R_L)$

Take the ratio of,  $V_1 / I_1$  ---1

Draw the circuit by inter changing position of  $V_1$  and  $I_1$



Find the total resistance of the circuit,  $R_t = (R_3+R_L) + [R_2(R_1)] / R_2+R_1$ .

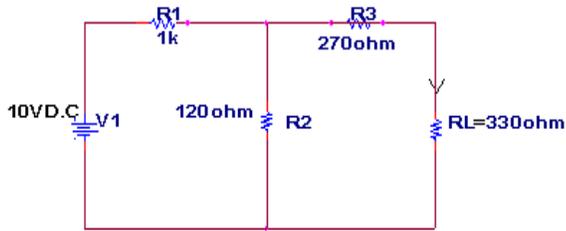
Hence source current,  $I = V_1 / R_t$ .

Current through  $R_L$  is  $I_1 = I \cdot R_2 / (R_2+R_1)$

Take the ratio of,  $V_1 / I_1$  ---2

If ratio 1 = ratio 2, then circuit is said to be satisfy reciprocity.

Eg: **With AC source**



:

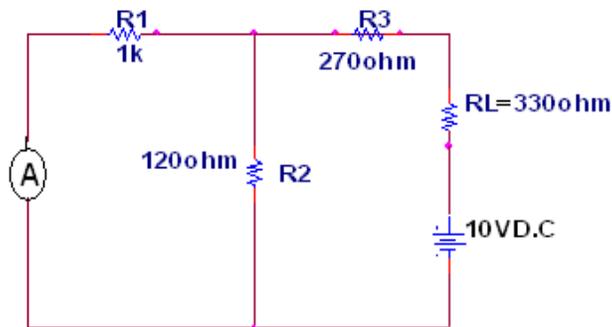
Find the total impedance of the circuit,  $Z_t = Z_1 + [Z_2(Z_3 + Z_L)] / Z_2 + Z_3 + Z_L$ .

Hence source current,  $I = V_1 / Z_t$ .

Current through  $Z_L$  is  $I_1 = I \cdot Z_2 / (Z_2 + Z_3 + Z_L)$

Take the ratio of,  $V_1 / I_1$  ---1

Draw the circuit by inter changing position of  $V_1$  and  $I_1$



Find the total impedance of the circuit,  $Z_t = (Z_3 + Z_L) + [Z_2(Z_L)] / Z_2 + Z_1$ .

Hence source current,  $I = V_1 / Z_t$ .

Current through  $Z_L$  is  $I_1 = I \cdot Z_2 / (Z_2 + Z_1)$

Take the ratio of,  $V_1 / I_1$  ---2

If ratio 1 = ratio 2, then circuit is said to be satisfy reciprocity.

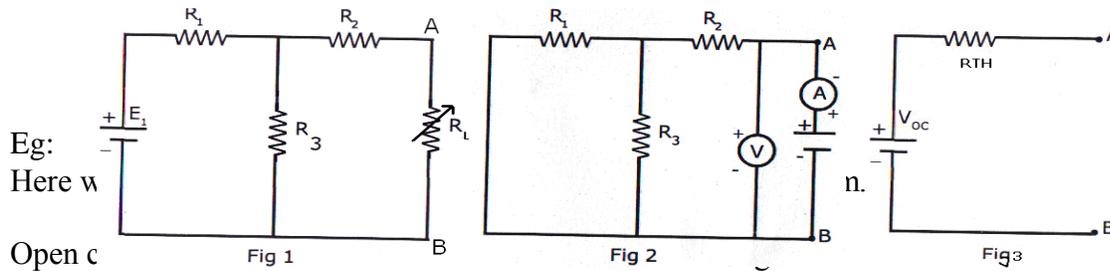
\*\*\* Here only magnitudes are compared.

#### 5.4 THEVENIN'S THEOREM:

**DC:** " An complex network consisting of number voltage and current sources can be replaced by simple series circuit consisting of equivalent voltage source in series with equivalent resistance, where equivalent voltage is called as open circuit voltage and equivalent resistance is

called as thevenin's resistance calculated across open circuit terminals while all energy sources are non-operative"

**AC:** " An complex network consisting of number voltage and current sources cand be replaced by simple series circuit consisting of equivalent voltage source in series with equivalent impedance, where equivalent voltage is called as open circuit voltage and equivalent impedance is called as thevenin's impedance calculated across open circuit terminals while all energy sources are non-operative"



Thevenin's voltage ,  $V_{th} = E1 \cdot R3 / (R1+R3)$  ----1 from figure .1

Thevenin's resistance,  $R_{th} = (R1 \cdot R3) / (R1+R3) + R2$  ----2 from figure 2.

Now draw the thevenin's equivalent circuit as shown in figure 3 with calculated values.

**Eg: With AC excitation**

Here we need to find current through  $Z_L$  using thevenin's theorem.

Open circuit the AB terminals to find the Thevenin's voltage.

Thevenin's voltage ,  $V_{th} = E1 \cdot R3 / (R1+R3)$  ----1 from figure .1

Thevenin's impedance,  $Z_{th} = (Z1 \cdot Z3) / (Z1+ Z3) + Z2$  ----2 from figure 2.

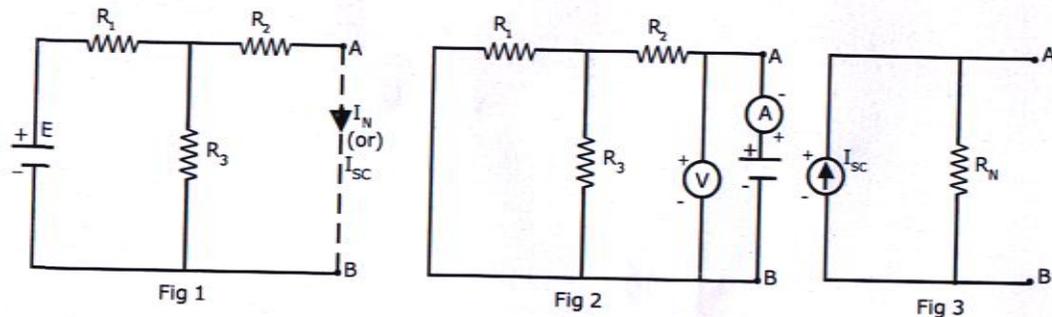
Now draw the thevenin's equivalent circuit as shown in figure 3 with calculated values.

## 5.5 NORTON'S THEOREM:

**DC:** " An complex network consisting of number voltage and current sources cand be replaced by simple parallel circuit consisting of equivalent current source in parallel with equivalent resistance, where equivalent current source is called as short circuit current and equivalent resistance is called as norton's resistance calculated across open circuit terminals while all energy sources are non-operative"

**AC:** "An complex network consisting of number voltage and current sources cand be replaced by simple parallel circuit consisting of equivalent current source in parallel with equivalent

impedance, where equivalent current source is called as short circuit current and equivalent impedance is called as norton's impedance calculated across open circuit terminals while all energy sources are non-operative"



Here we need to find current through RL using norton's theorem.

Short circuit the AB terminals to find the norton's current.

Total resistance of circuit is,  $R_t = (R_2 \cdot R_3) / (R_2 + R_3) + R_1$

Source current,  $I = E / R_t$

Norton's current,  $I_N = I \cdot R_3 / (R_2 + R_3)$  ----1 from figure .1

Norton's resistance,  $R_N = (R_1 \cdot R_3) / (R_1 + R_3) + R_2$  ----2 from figure 2.

Now draw the Norton's equivalent circuit as shown in figure 3 with calculated values.

**Eg: With AC excitation**

Here we need to find current through ZL using norton's theorem.

Short circuit the AB terminals to find the norton's current.

Total impedance of circuit is,  $Z_t = (Z_2 \cdot Z_3) / (Z_2 + Z_3) + Z_1$

Source current,  $I = E / Z_t$

Norton's current,  $I_N = I \cdot Z_3 / (Z_2 + Z_3)$  ----1 from figure .1

Norton's impedance,  $Z_N = (Z_1 \cdot Z_3) / (Z_1 + Z_3) + Z_2$  ----2 from figure 2.

Now draw the Norton's equivalent circuit as shown in figure 3 with calculated values.

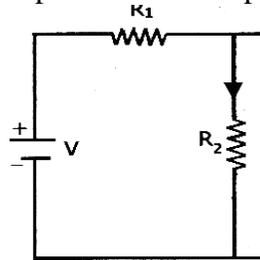
\*\*\* These two theorems are useful in determining the load value for which maximum power transfer can be happened.

## 5.6 MAXIMUM POWER TRANSFER THEOREM:

**DC:** “ In linear bi-lateral network maximum power can be transferred from source to load if load resistance is equal to source or thevenin’s or internal resistances”.

**AC:** “ In linear bi-lateral network maximum power can be transferred from source to load if load impedance is equal to complex conjugate of source or thevenin’s or internal impedances”

Eg: For the below circuit explain maximum power transfer theorem.



Let I be the source current,  $I = V / (R1+R2)$

Power absorbed by load resistor is,  $PL = I^2 \cdot R2$

$$= [ V / (R1+R2)]^2 \cdot R2.$$

To say that load resistor absorbed maximum power ,  $dPL / dR2 = 0$ .

When we solve above condition we get,  $R2 = R1$ .

Hence maximum power absorbed by load resistor is,  $PL_{max} = V^2 / 4R2$ .

Eg: **AC excitation**

Let I be the source current,  $I = V / (Z1+ Z 2)$

Power absorbed by load impedance is,  $PL = I^2 \cdot Z2$

$$= [ V / (Z1+ Z2)]^2 \cdot Z2.$$

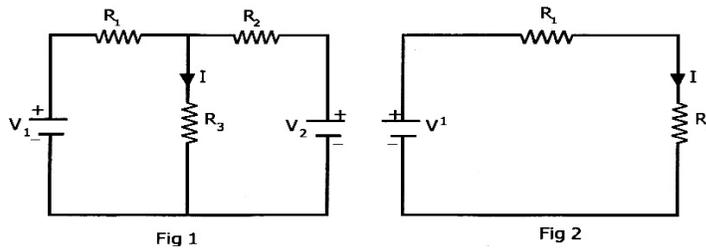
To say that load resistor absorbed maximum power ,  $dPL / d Z2 = 0$ .

When we solve above condition we get,  $Z2 = Z1^*$  .

Hence maximum power absorbed by load resistor is,  $PL_{max} = V^2 / 4 Z2$ .(magnitude)

### 5.7 MILLIMAN'S THEOREM:

**DC:** “ An complex network consisting of number of parallel branches , where each parallel branch consists of voltage source with series resistance, can be replaced with equivalent circuit consisting of one voltage source in series with equivalent resistance”



Where equivalent voltage source value is ,  $V' = \frac{(V1G1+V2G2+\dots+VnGn)}{G1+G2+\dots+Gn}$

Equivalent resistance is ,  $R' = 1 / ( G1+G2+\dots+Gn)$

**AC:** “ An complex network consisting of number of parallel branches , where each parallel branch consists of voltage source with series impedance, can be replaced with equivalent circuit consisting of one voltage source in series with equivalent impedance”

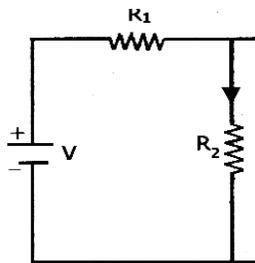
Where equivalent voltage source value is ,  $V' = \frac{(V1Y1+V2Y2+\dots+VnYn)}{Y1+Y2+\dots+Yn}$

Equivalent resistance is ,  $Z' = 1 / ( Y1+Y2+\dots+Yn)$

\*\*\* It is also useful in designing load value for which it absorbs maximum power.

### 5.8 COMPENSATION THEOREM:

**DC & AC:** “ compensation theorem states that any element in the network can be replaced with Voltage source whose value is product of current through that element and its value”  
It is useful in finding change in current when sudden change in resistance value.



For the above circuit source current is given as,  $I = V / (R_1 + R_2)$

Element  $R_2$  can be replaced with voltage source of,  $V' = I \cdot R_2$

Let us assume there is change in  $R_2$  by  $\Delta R$ , now source current is  $I' = V / (R_1 + R_2 + \Delta R)$

Hence actual change in current from original circuit to present circuit is  $= I - I'$ .

This can be find using compensation theorem as, making voltage source non-operative and replacing  $\Delta R$  with voltage source of  $I' \cdot \Delta R$ .

Then change in current is given as  $= I' \cdot \Delta R / (R_1 + R_2)$